

**Preston New Road 1z  
Hydraulic Fracture Plan**



<b>Well Classification:</b>	Exploration Onshore Horizontal Well
<b>Well Name:</b>	Preston New Road-1z
<b>Operator:</b>	Cuadrilla Bowland Ltd
<b>Licence:</b>	EXL269 (for site location), PEDL165 (for lateral well)
<b>Partners:</b>	PEDL165 Cuadrilla Resources Ltd – 51.25% Centrica- 25% AJ Lucas – 23.75% EXL269 Cuadrilla Resources Ltd – 50.1875%; Centrica – 22.75%, AJ Lucas 22.0625%, Warwick Energy - 5%
<b>Expected Lateral Length [TVD]</b>	1000 m [2180 m TVD]
<b>Surface Coordinates:</b>	Northing 432749.50 m Easting 337433.54 m [BNG - OSGB36] Lat 53° 47' 14.2827" N Long 02° 57' 04.0278" W [WGS84]
<b>TD Coordinates:</b>	Northing 432749.5m Easting 335620.70m [BNG - OSGB36] Lat 53° 47' 13.4857" N Long 02° 58' 43.0676" W [WGS84]

<b>Local Faulting</b>	Type   Distance to nearest injection point	Dip   Strike   Throw
Moor Hey	Reverse   1200 m	53°E   041°   730 m
Anna's Road	Reverse   650 m	40°E   061°   650 m
Haves Ho	Reverse   1300 m	50°E   044°   1700 m
PNR-1	Reverse   500 m	60°E   019°   200 m
Fault-2	Reverse   1200 m	85°E   032°   30 m
Thistleton	Normal   2300 m	68°E   030°   850 m

<b>Seismic Discontinuities</b>	Type   Distance to nearest injection point	Dip   Strike   Throw
SD1	Reverse   200 m	53°E   021°   30 m
SD2	Reverse   600 m	73°E   070°   40 m
SD3	Normal   0 m	75°E   150°   25 m
SD4	Reverse   100 m	42°E   033°   25 m
SD5	Reverse   200 m	50°E   022°   20 m
SD6	Normal   550 m	67°E   030°   60 m

<b>Stress Analysis</b>	Regional SHmax azimuth 173° (NNW-SSE) strike slip regime
Shmax	2.82 SG (23.5 ppg) EMW <sup>(1)</sup>
SHmin	1.72 SG (14.3 ppg) EMW <sup>(1)</sup>
Background Seismicity Results	12 months monitoring via 7 broadband seismometers. No seismicity within permitted boundary (19 events from 0.7-4.2 M <sub>L</sub> detected outside the permitted boundary   Nearest event @ 36 km). Data provided to the BGS. <sup>(2)</sup>
Induced Seismicity Risk	The effects of induced seismicity associated with the project are not significant. The potential cumulative effects have also been addressed as not significant. See the PNR ES Chapter 12 <sup>(10)</sup> for more detail.

<b>Previous and Planned Operations</b>	Elswick-1	Preese Hall-1	Preston New Road-1z
Well Type	Vertical	Vertical	Horizontal
Fluid Type	Gelled-water with CO <sub>2</sub>	Slickwater	Slickwater
Stages	1	5	Up to 45
Hydraulic Fracturing Fluid Volume per Stage	163 m <sup>3</sup> water, 24.3 t CO <sub>2</sub>	Maximum 2339 m <sup>3</sup>	Up to 765 m <sup>3</sup>
Proppant Volume per Stage	58.5 t	Maximum 116.6 t	50 t
Seismic Monitoring		BGS Network <sup>(11)</sup>	BGS Network
			Local real time 8 station array
			Real time downhole microseismic monitoring array
Pre Operational Investigations	2D Seismic Interpretation	2D Seismic Interpretation	3D Seismic Interpretation <sup>(12)</sup>
Historic Seismicity	None noted	1.5 & 2.3 (M <sub>L</sub> ) Induced <sup>(11)(4)</sup>	None noted within permitted boundary during 12 months monitoring <sup>(2)</sup>

<b>Proposed Injection Design</b>	Slickwater   Sliding sleeve   Coil tubing
Injection / Stage	Up to 765 m <sup>3</sup> (Schedule 3 Table S3.2 EPR/AB3101MW) <sup>(5)</sup>
Proppant / Stage	Up to 75 t proppant per stage   100 mesh Congleton sand and 30/50 mesh Chelford sand <sup>(6)</sup>
Additives	Polyacrylamide based friction reducer (maximum concentration 0.05%)   <10% HCl up to 3 m <sup>3</sup> per stage   UV in event of reuse   (As required in Schedule 1 A5 EPR/AB3101MW) <sup>(5)</sup>
Estimated Pumping Pressure / Rate	Surface 51.7 Mpa [7500 psi] - 3.6 m <sup>3</sup> /minute
Maximum Pumping Pressure / Rate	Surface 65.5 Mpa [9500 psi] - 6.375 m <sup>3</sup> /minute (Schedule 3 Table S3.2 (EPR/AB3101MW)) <sup>(5)</sup>
Wellbore Deviation Plan / Injection Points	See Appendix 3

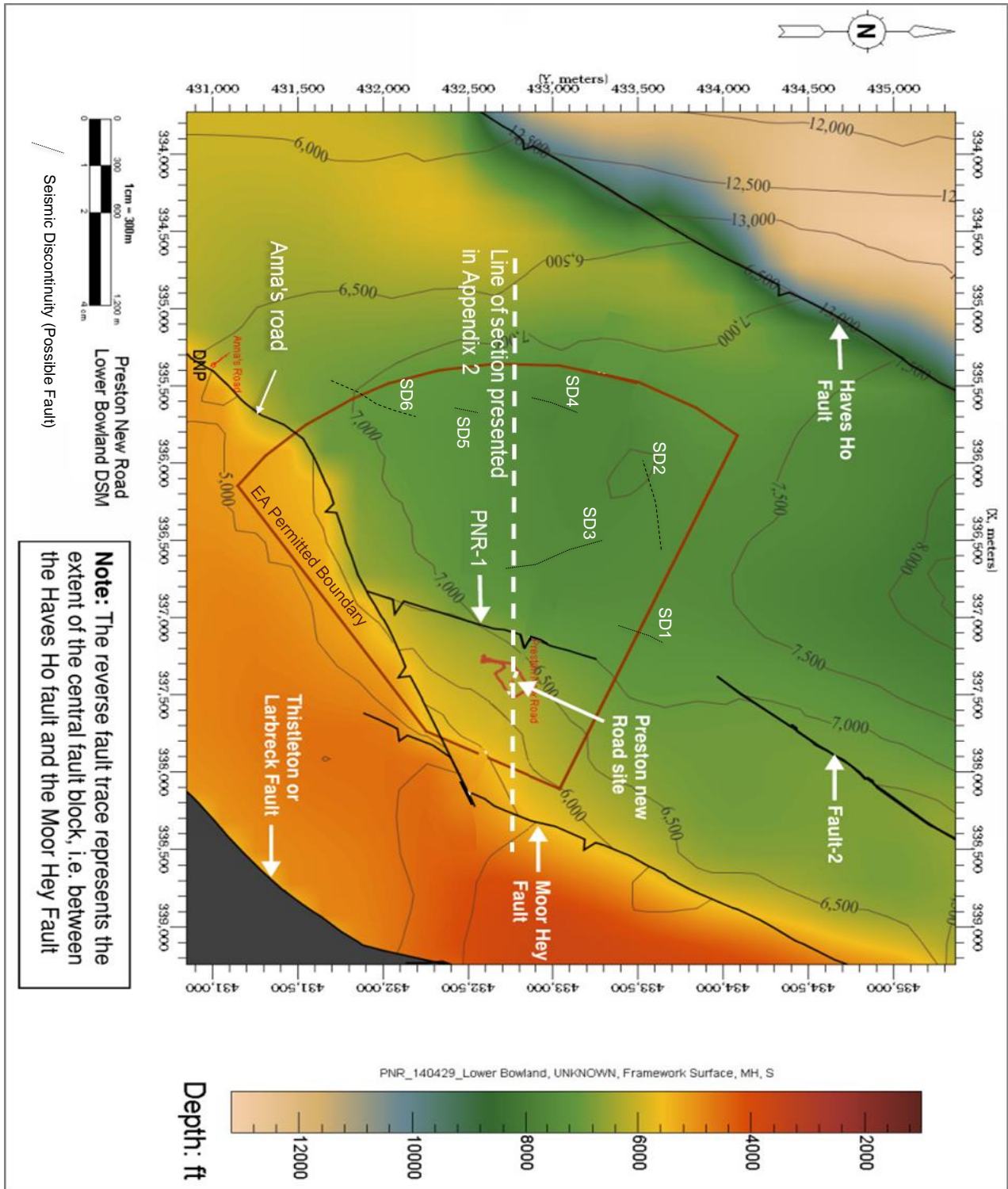
<b>Fracture Modelling</b>	P3D simulation model of planer propagation based on PH-1 geology		
	400 m <sup>3</sup> stage size	600 m <sup>3</sup> stage size	765 m <sup>3</sup> stage size
Fracture Total Height	78 m	85 m	133 m
Fracture Half Length	36 m	34 m	31 m

<b>Mitigation Methods / Monitoring</b>	TLS   Microseismic   Vibration		
Traffic Light System (TLS)	8 real time seismometers installed <sup>(13)</sup>	Combination of broadband seismometers and 4.5 Hz, 3 component geophones. Minimum of 6 required for operational TLS. <sup>(15)</sup>	Estimated detectability -0.5 (M <sub>L</sub> ), accuracy 300 m (X,Y) 300 m (Z) at estimated injection depth
TLS Monitoring Duration	Monitored 4 weeks before and 2 weeks after injection operations. During operations (24 hours) <sup>(13)</sup> .		

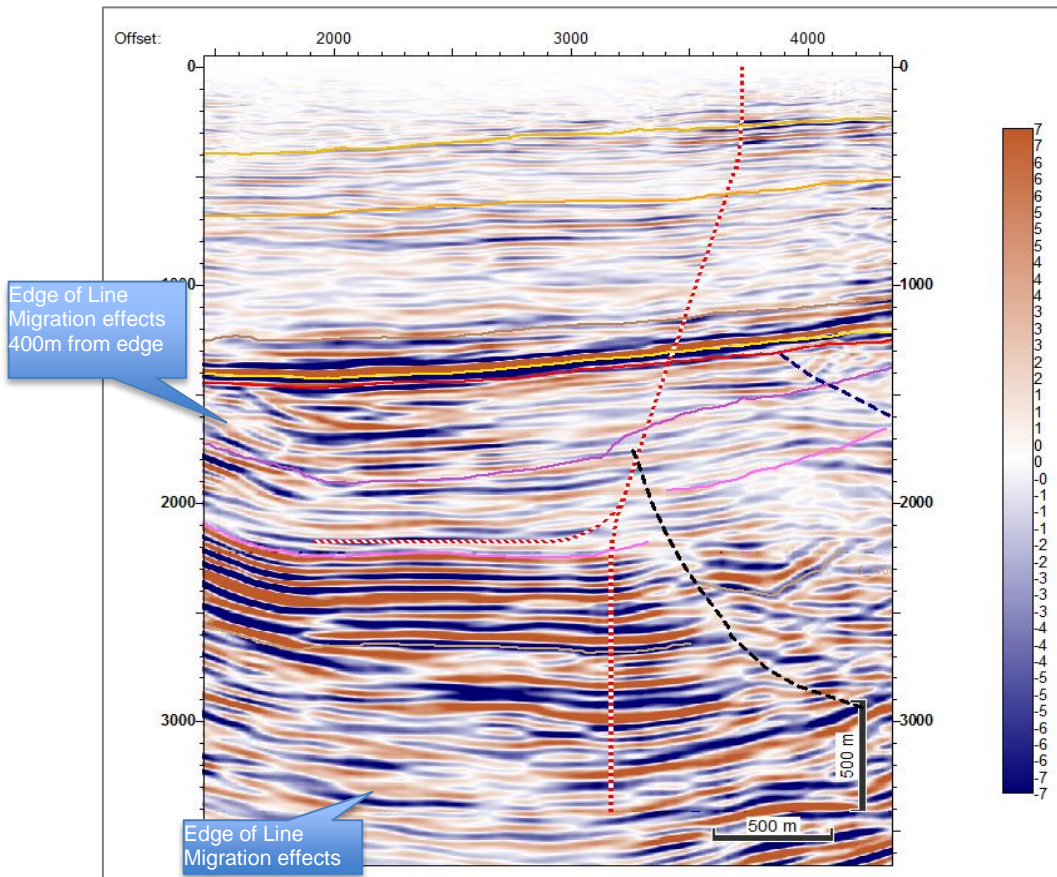
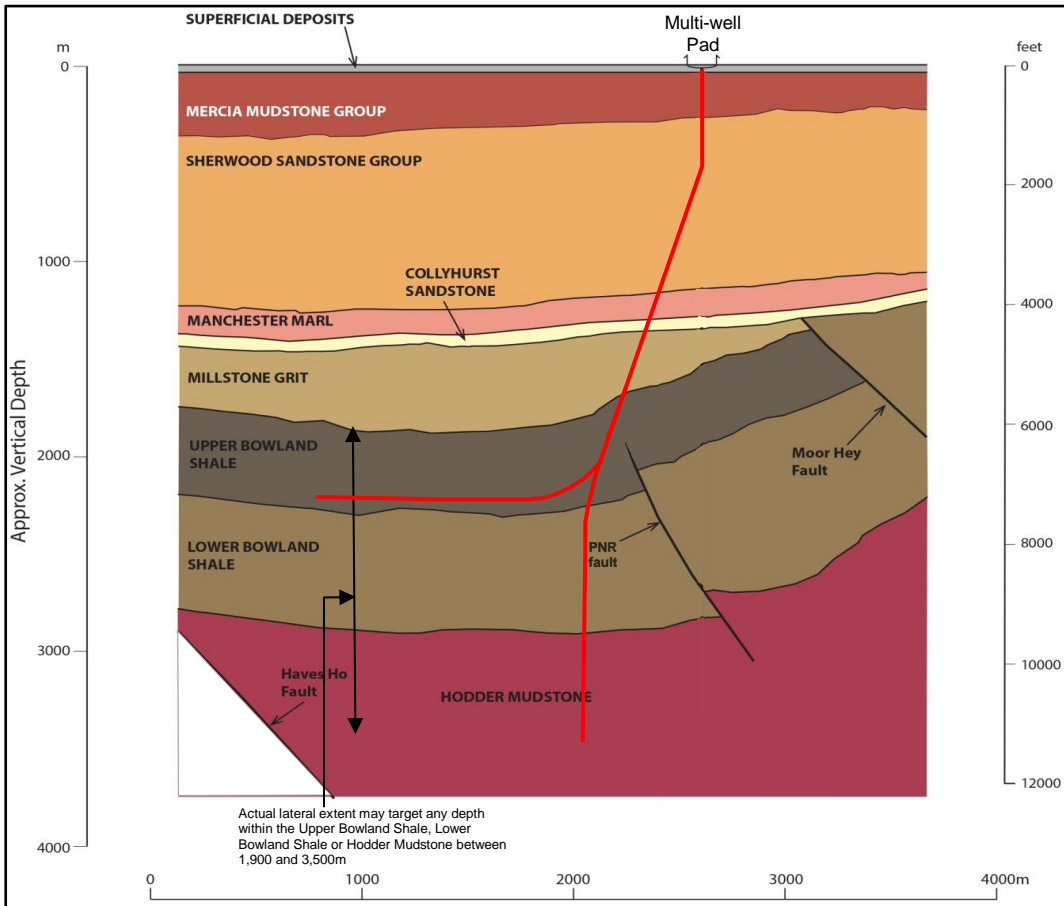
# Preston New Road 1z Hydraulic Fracture Plan



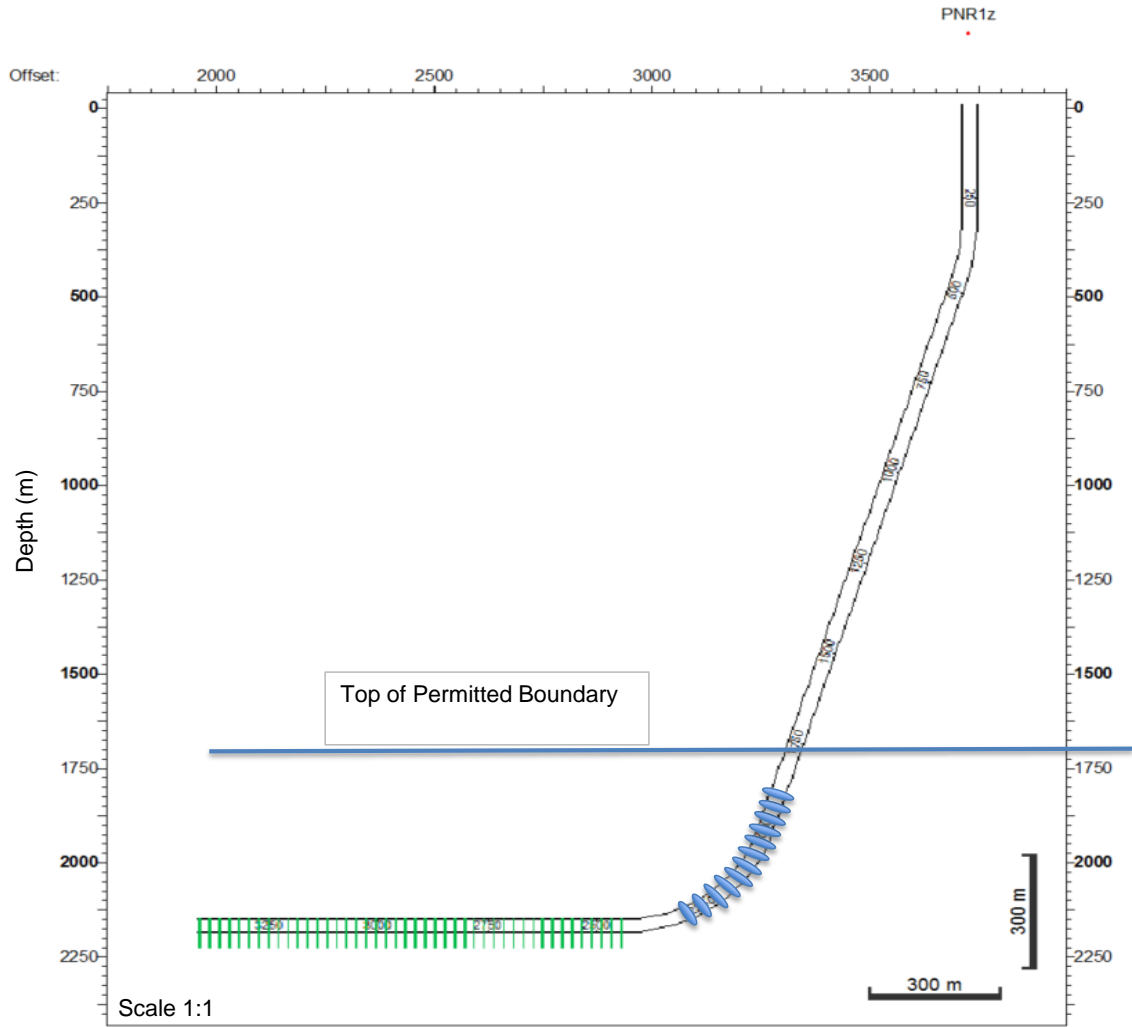
TLS Array Location	Instruments installed in an array from 1.0 km to 3.9 km from the site and have been independently assessed as to quantity, location and redundancy <sup>(13)</sup> .		
TLS Decision Tree	<a href="#">See Appendix 4</a>		
Vibration Monitoring System	Minimum of 4 peak partial velocity (PPV) monitors active in addition to PPV data from 8 TLS stations		
Vibration Monitoring Duration	Monitored before and after operations (2 weeks). During operations (24 hours)		
Vibration Monitoring Decision tree	<a href="#">See Appendix 4</a>		
Microseismic Array / Fracture Mapping	Real Time Downhole Microseismic Monitoring Array	12 slim hole, 3 component, 15 Hz Geophones	Estimated detectability -1.8 (M <sub>L</sub> ), accuracy 20 m (X,Y) 20 m (Z) at the toe of the well
Microseismic Duration	Real time monitoring throughout pumping operations		
Operational Boundary	Within the areal extent of the TLS		
Assurance	Microseismic monitoring will be installed and executed by a competent contractor specialising in microseismic monitoring. The contractor will follow its own quality assurance procedures for calibration and data gathering.		
Microseismic Monitoring / Induced Seismicity Mitigation	<p>The HFP applies an evolutionary approach to risk assessment and mitigation (operational mitigation) <sup>(10)</sup>. This stepped progressive approach to hydraulic fracturing will consist of an initial mini-fracture stage and modest initial pumped volumes, building up to a maximum pump volume of 765 m<sup>3</sup> per stage. As this process continues, an understanding of the performance of the reservoir during hydraulic fracturing is developed by;</p> <p>1) Monitoring the extent of fracture growth using a real time downhole microseismic array. If, during hydraulic fracturing, monitoring data indicates possible fault interactions with a preferential flow pathway, the pumping of fracturing fluid would be adjusted or terminated and the HFP would be modified as necessary.</p> <p>2) Implementation of the Traffic Light System. As long as the induced seismicity is &lt;0.0M<sub>L</sub> (Green level) while pumping, operations will continue. If an induced seismicity event occurs in the range of ≥0ML to &lt;0.5ML (Amber level) while pumping, the fracture stage can be completed. On completion of the injection the flowback procedure will be initiated. Pumping may then proceed with caution, possibly at reduced parameters. If an event occurs that is ≥0.5ML (Red level) while pumping, the fracture stage will be aborted and the flush and flowback procedure will be initiated. Should seismicity occur at or above the red 0.5 M<sub>L</sub> level then a vibration monitoring array will be utilised to assess the impact in accordance with BS7358-2. The measurement recorded by the vibration monitoring array and traffic light system will then be used to assess the calibration of the ground motion prediction model <sup>(14)</sup> and amendments applied if required. Cuadrilla are anticipating that the horizontal well bore, or the area intended to be hydraulically stimulated, will encounter a number of small faults. <sup>(9)</sup> Modelling a worst case scenario (direct injection into a predicted or unpredicted critically stressed fault) and using 2000 m<sup>3</sup> stages the upper bound estimate for maximum magnitude possible would be 3.1 M<sub>L</sub> <sup>(6)</sup>, which is considered to be a very low likelihood <sup>(10)</sup>. If vibration occurs in excess of 3.1M<sub>L</sub> and or PPV of 15 mm/s (as referenced in BS7358-2) due to injective operations, which is considered to be a very low likelihood, then future injection operations will be altered to mitigate below the PPV 15 mm/s level by adjusting fluid volume, rate, pressure, and or injection point. Where possible TLS data will be co-processed with any available BGS data, event magnitude determination will be calculated using the BGS methodology.</p>		
Permit Boundary / Microseismic Monitoring	<p>An evolutionary process as described in the PNR ES Chapter 12 <sup>(10)</sup> will be employed to understand the performance of the reservoir during fracturing. This stepped progressive approach to hydraulic fracturing will consist of an initial mini-fracture stage and modest initial pumped volumes building up to a maximum pump volume of 765 m<sup>3</sup> per stage. As this process continues, an understanding of the performance of the reservoir during hydraulic fracturing is developed by monitoring the extent of fracture growth using a real time downhole microseismic array. If, during hydraulic fracturing, monitoring data indicate possible fracture growth with a preferential flow pathway towards the edge of the permitted boundary the pumping of fracturing fluid would be adjusted or terminated and the HFP would be adjusted as necessary to prevent future occurrences. If fracture fluid is interpreted (by an agreed methodology with the Environment Agency) to be outside of the permitted boundary injection will stop after flushing the well. Future injection operations will be altered to comply with the permitted boundary by adjusting fluid volume, rate, pressure, and or injection point.</p>		
Groundwater Monitoring	<p>The Waste Management Plan (HSE-Permit-INS-PNR-006) details groundwater monitoring approach and protection measures.</p> <p>Further details have been submitted and approved in PO4 and PO7 which provides groundwater borehole installation and monitoring. The frequency of monitoring is outlined within the Permit EPR/ AB3101MW.</p>		
<b>Reporting</b>	TLS status reported without delay on Cuadrilla e-portal		
Morning Report	Submitted daily during fracturing operations. Injection depth. Volumes and type of water, proppant, chemicals pumped. Schematic of fracture growth, including the location, orientation and extent of the induced fractures, in relation to permitted boundary. Proposed mitigation measures if required. Induced seismicity of note.		
Post Frac Reporting	End of Well Report as per PON9b Quarterly report as per S4.1 (EPR/AB3101MW)		
<b>Seismic Level Requiring Integrity Check</b>	<a href="#">See Appendix 4</a>		
<b>Verification Updates</b>	Provided to the EA, OGA, HSE		
On TD of Pilot Well	Formation tops, stress azimuth.		
On Completion of Lateral Well	Deviation profile, target formation, injection points.		
<b>References / Related Documents</b>	<ol style="list-style-type: none"> <li>1: PNR Environmental Statement - Appendix L Fig. 12</li> <li>2: <a href="http://www.bgs.ac.uk/research/groundwater/shaleGas/monitoring/seismicity.html">http://www.bgs.ac.uk/research/groundwater/shaleGas/monitoring/seismicity.html</a></li> <li>3: de Pater, H. &amp; Baisch, S. 2011. Geomechanical Study of Bowland Shale Seismicity, Synthesis Report</li> <li>4: Clarke, H., Eisner, L., Styles, P. and Turner, P. 2014. Felt seismicity associated with shale gas hydraulic fracturing: The first documented example in Europe, Geophysics. Res. Lett., 41, 23, 8308-8314.</li> <li>5: Preston New Road Exploration Site Permit numbers EPR/AB3101MW</li> <li>6: PNR Environmental Statement - Appendix B7</li> <li>7: PNR Environmental Statement - Chapter 12</li> <li>8: de Pater, C.J. &amp; Baisch, S., 2011. Geomechanical Study of Bowland Shale Seismicity. Synthesis Report. For Cuadrilla Resources Ltd. 57pp. - Section 6.</li> <li>9: PNR Environmental Statement - Chapter 12, para156</li> <li>10: PNR Environmental Statement - Chapter 12, Summary</li> <li>11: <a href="http://earthquakes.bgs.ac.uk/research/earthquake_hazard_shale_gas.html">http://earthquakes.bgs.ac.uk/research/earthquake_hazard_shale_gas.html</a></li> <li>12: PNR Environmental Statement - Appendix L10.2.2</li> <li>13: PNR Environmental Statement - Appendix L10.7</li> <li>14: PNR Environmental Statement - Appendix L8.2.2</li> <li>15: PNR Environmental Statement - Appendix L10.8.01</li> </ol>		



Appendix 2 Seismic Cross Section

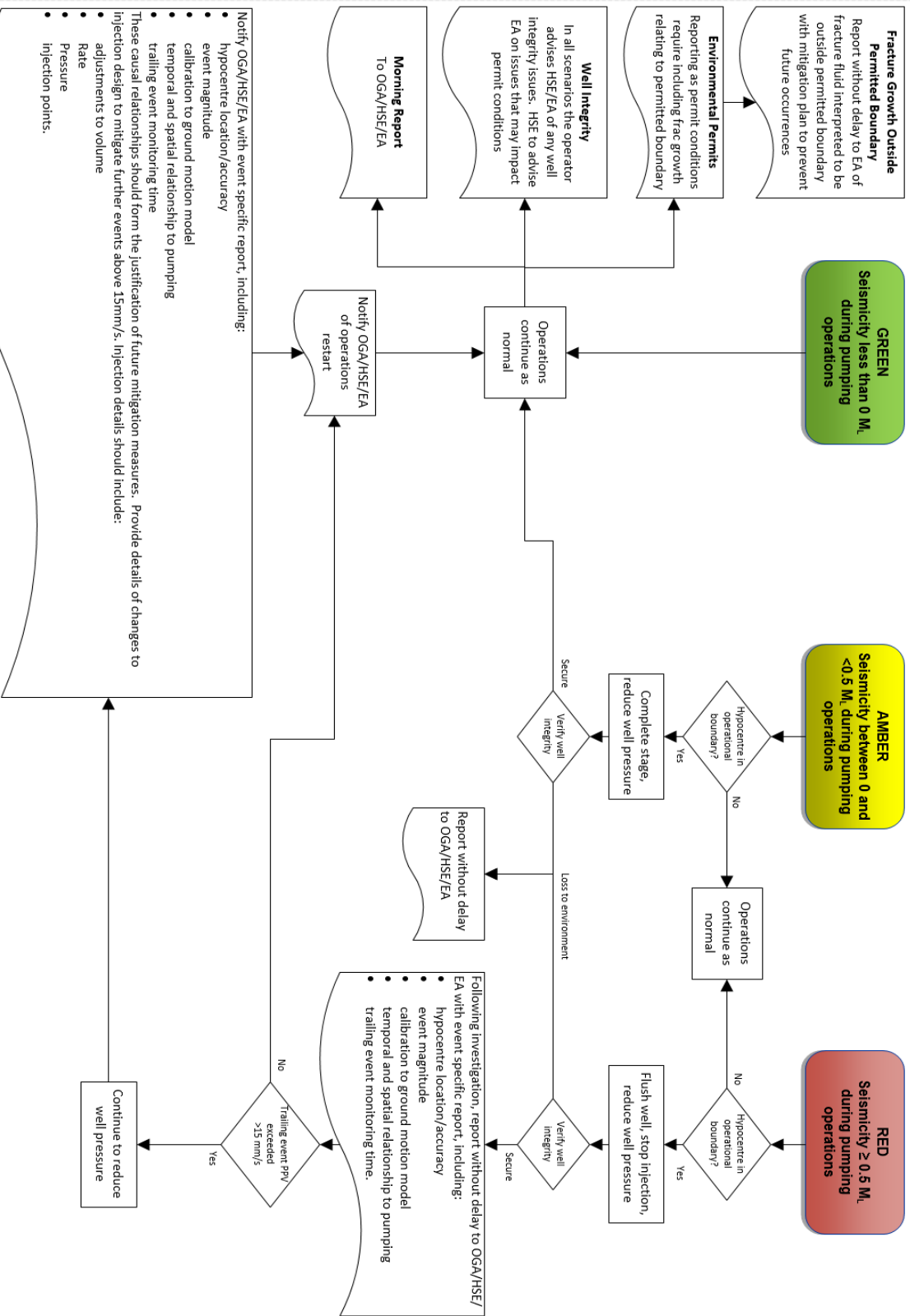


**Appendix 3** Wellbore profile, hydraulic injection Locations, indicative microseismic array position  
 Note: microseismic monitoring will be performed from the observation well, not injection well.



Key: Green Injection points  
 Blue Microseismic observation points

# HVHF Pumping Traffic Light and Surface Vibration System



BGS	British Geological Survey
EA	Environment Agency
EMW	equivalent mud weight
ES	environment statement
ft	feet
HCl	hydrochloric acid
Km	kilometres
Lat	Latitude
Long	Longitude
m	metres
m <sup>3</sup>	cubic metres
MD	measured depth
M <sub>L</sub>	local magnitude scale
mm/sec	millimetres per second
Mpa	megapascals
OGA	Oil and Gas Authority
PH	Preese Hall
PNR	Preston New Road
ppg	pounds per gallon
PPV	peak particle velocity
psi	pounds per square inch
SG	specific gravity
SHmax	maximum horizontal stress
Shmin	mininum horizontal stress
t	tonnes
TD	total depth
TLS	traffic light system
TVD	true vertical depth

OGA, EA Guidance

Required Item	Location in HFP
Map and seismic lines showing faults near the well and along the well path.	<a href="#">Appendix1 - Lower Bowland Depth Structure Map</a>
Summary assessment of faulting and formation stresses in the area and the risk that the operations could reactivate existing faults	<a href="#">Local Faulting</a> <a href="#">Stress Analysis</a>
Information on the local background seismicity	<a href="#">Background Seismicity Results</a>
Assessment of the risk of induced seismicity	<a href="#">Induced Seismicity risk</a>
Comparison of proposed activity to any previous operations and relationship to historical seismicity	<a href="#">Previous Operations</a>
Summary of the planned operations, including the techniques to be used, stages, pumping pressures, volumes and the predicted extent of each proposed fracturing event	<a href="#">Proposed Injection Design</a>
Summary of the planned operations - the location of monitoring points	<a href="#">TLS Array Location</a>
Proposed measures to mitigate the risk of inducing an earthquake	<a href="#">Mitigation Methods/Monitoring</a>
Description of decision tree for a real-time traffic light scheme for monitoring local seismicity	<a href="#">Appendix 4 - TLS and Vibration Monitoring Decision Tree</a>
The processes and procedures that will be put in place during hydraulic fracturing for fracture height monitoring to identify where the fractures are within the target formation and ensure that they are not near the permitted boundary	<a href="#">Microseismic Array/Fracture Mapping</a> <a href="#">Permit Boundary/Microseismic Monitoring</a>
In the event that the fractures extend beyond the EA permit boundary, the steps that would be taken to assess and if necessary mitigate the effect and limit further propagation outside the target rocks	<a href="#">Permit Boundary/Microseismic Monitoring</a>
The type and duration of monitoring and reporting during and/or after hydraulic fracturing has taken place and the geologic data to be published	<a href="#">Vibration Monitoring Duration</a>
Procedure for post fracturing reporting of the location, orientation and extent of the induced fractures to demonstrate that the EA permit has been complied with. This will need to include provision for reporting on proposed mitigation measures to prevent propagation should fractures extend to within a short distance of the permitted boundary	<a href="#">Reporting</a>
Proposed level of seismic event above which fracturing cannot resume without consent after evidence is provided that the wells are not damaged and the groundwater remains protected	<a href="#">Seismic Level Requiring Integrity Check</a>